

REFERENCES

1. A. J. Wagner, "The Weather and Circulation of September 1967—A Month of Continued Record Warmth in the West, Coolness in the East, and Frequent Tropical Activity," *Monthly Weather Review*, vol. 95, No. 12, Dec. 1967, pp. 956-966.
2. Environmental Data Service, ESSA, *Weekly Weather and Crop Bulletin*, vol. 54, Nos. 41-45, Oct. 9, 16, 23, 30, and Nov. 6, 1967, pp. 1-8.

CORRECTION NOTICE

Vol. 95, No. 9, pp. 615-626: Data in tables 3-6 inadvertently repeat the data in table 2. We regret the inconvenience this error may have caused users of these data. Corrected tables 3-6 are presented on the following pages (pp. 63-74).

TABLE 3.—Computed wind stresses, March-April-May. Upper number = τ_x , lower number = τ_z , in 10^{-2} dynes cm^{-2}

TABLE 3.—Continued

TABLE 3.—Concluded

| | 117.5W | 107.5 | 97.5 | 87.5 | 77.5 | 67.5 | 57.5 | 47.5 | 37.5 | 27.5 | 17.5 | 7.5W |
|-------|--------|-------|------|------|------|------|------|------|------|------|------|------|
| 72.5N | • | • | • | • | • | • | -28 | -24 | • | • | • | -78 |
| 67.5N | • | • | • | • | • | • | -28 | -31 | -24 | • | • | -75 |
| 62.5N | • | • | • | • | • | • | -20 | -7 | -10 | • | -17 | -14 |
| 57.5N | • | • | • | • | • | • | -18 | -29 | -24 | -39 | 51 | -3 |
| 52.5N | • | • | • | • | • | • | • | 15 | 21 | 4 | 48 | -12 |
| 42.5N | • | • | • | • | • | • | 80 | 68 | 61 | 51 | 84 | 40 |
| 37.5N | • | • | • | • | • | 49 | 54 | 70 | 53 | 62 | 80 | 28 |
| 32.5N | • | • | • | • | • | 11 | 25 | 39 | 31 | 49 | 23 | 20 |
| 27.5N | • | • | • | • | • | -38 | 7 | -10 | -12 | -15 | -17 | -11 |
| 22.5N | -33 | -1 | • | • | • | -32 | -41 | -38 | -41 | -30 | -48 | -14 |
| 17.5N | -76 | • | • | • | • | -24 | -31 | -25 | -15 | -12 | -20 | -10 |
| 12.5N | -43 | -1 | -10 | -14 | -13 | -10 | -14 | -12 | -12 | -15 | -14 | -11 |
| 7.5N | -55 | -18 | -18 | -9 | -5 | -37 | -22 | -24 | -21 | -21 | -26 | -23 |
| 2.5N | -37 | -18 | -10 | -13 | -8 | -10 | -13 | -9 | -14 | -14 | -14 | -14 |
| 2.5S | -49 | -17 | -10 | -13 | -7 | -17 | -20 | -16 | -16 | -16 | -16 | -16 |
| 7.5S | -62 | -56 | -60 | -50 | -62 | -50 | -52 | -52 | -53 | -53 | -53 | -53 |
| 12.5S | -65 | -72 | -81 | -65 | -61 | -63 | -53 | -55 | -57 | -57 | -57 | -57 |
| 17.5S | -49 | -51 | -50 | -55 | -54 | -59 | -40 | -31 | -7 | -19 | -31 | -19 |
| 22.5S | -31 | -17 | -37 | -34 | -23 | -29 | -28 | -19 | -20 | -21 | -23 | -23 |
| 27.5S | -44 | 4 | -5 | 4 | -1 | 40 | 41 | 22 | 14 | 15 | 10 | -5 |
| 42.5S | 107 | 140 | 191 | 179 | 181 | 152 | 172 | 165 | 155 | 142 | 123 | 106 |
| 47.5S | 191 | 193 | 203 | 205 | 209 | 299 | 294 | 215 | 144 | 132 | 79 | 156 |
| 52.5S | 192 | 194 | 200 | 224 | 298 | 309 | 277 | 317 | 154 | 155 | 137 | 209 |
| 57.5S | 140 | 141 | 1 | 1 | 8 | 19 | 198 | 237 | 271 | 241 | 226 | 164 |
| 62.5S | • | • | • | • | • | 114 | 118 | 120 | 110 | 91 | 76 | 33 |
| 67.5S | • | • | • | • | • | 112 | 122 | 137 | 138 | 109 | 82 | • |

TABLE 4.—Computed wind stresses, June-July-August. Upper number = τ_u , lower number = τ_v in 10^{-2} dynes cm. $^{-2}$

TABLE 4.—Continued

| | 122.5E | 132.5 | 142.5 | 152.5 | 162.5 | 172.5E | 177.5W | 167.5 | 157.5 | 147.5 | 137.5 | 127.5W |
|-------|--------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|--------|
| 72.5N | • | • | • | • | -17 | -29 | -36 | -29 | -32 | • | -11 | -8 |
| 67.5N | • | • | • | • | • | • | • | • | -13 | -8 | • | -16 |
| 62.5N | • | • | • | • | • | • | • | -4 | -12 | -11 | • | • |
| 57.5N | • | • | • | • | • | 21 | 14 | 14 | 13 | 12 | 14 | 16 |
| 52.5N | • | • | • | • | 12 | 17 | 23 | 23 | 25 | 26 | 26 | 20 |
| 47.5N | • | • | • | 15 | 16 | 10 | 14 | 9 | 15 | 16 | 18 | 16 |
| 42.5N | • | • | • | 15 | 12 | 8 | 20 | 26 | 34 | 37 | 33 | 37 |
| 37.5N | • | • | • | 22 | 20 | 12 | 17 | 20 | 24 | -10 | 12 | 17 |
| 32.5N | • | • | • | 22 | 28 | -12 | -10 | -7 | -11 | -13 | -10 | -17 |
| 27.5N | • | • | • | 25 | 24 | -32 | -23 | -29 | -30 | -31 | -32 | -33 |
| 22.5N | • | • | • | 27 | 22 | -32 | -28 | -23 | -19 | -13 | -12 | -11 |
| 17.5N | • | • | • | 25 | 24 | -33 | -36 | -35 | -32 | -30 | -29 | -28 |
| 12.5N | • | • | • | 26 | 24 | -34 | -35 | -32 | -26 | -22 | -25 | -27 |
| 7.5N | • | • | • | 19 | 17 | -19 | -14 | -11 | -13 | -12 | -13 | -14 |
| 2.5N | • | • | • | 13 | 12 | -13 | -14 | -11 | -10 | -9 | -10 | -11 |
| 7.5S | • | • | • | 91 | 52 | -91 | -52 | -43 | -48 | -62 | -53 | -54 |
| 12.5S | • | • | • | 44 | 31 | -44 | -31 | -23 | -30 | -33 | -35 | -36 |
| 27.5S | • | • | • | 43 | 46 | -60 | -60 | -73 | -70 | -142 | -64 | -46 |
| 17.5S | • | • | • | 40 | 43 | -63 | -60 | -46 | -72 | -20 | -23 | -24 |
| 22.5S | • | • | • | 42 | 37 | -59 | -54 | -54 | -51 | -56 | -51 | -52 |
| 27.5S | • | • | • | 43 | 46 | -60 | -60 | -73 | -70 | -142 | -64 | -46 |
| 32.5S | • | • | • | 42 | 37 | -59 | -54 | -54 | -51 | -56 | -51 | -52 |
| 37.5S | • | • | • | 45 | 39 | -53 | -43 | -39 | -35 | -31 | -35 | -36 |
| 42.5S | • | • | • | 45 | 50 | 43 | 33 | 24 | 1 | 14 | 22 | 25 |
| 47.5S | • | • | • | 48 | 82 | 107 | 100 | 98 | 107 | 94 | 60 | 49 |
| 52.5S | • | • | • | 148 | 144 | 126 | 111 | 161 | 182 | 136 | 119 | 81 |
| 57.5S | • | • | • | 190 | 140 | 116 | 105 | 105 | 132 | 129 | 138 | 140 |
| 62.5S | • | • | • | 190 | 140 | 116 | 105 | 105 | 132 | 129 | 138 | 140 |
| 67.5S | • | • | • | 190 | 140 | 116 | 105 | 105 | 132 | 129 | 138 | 140 |

TABLE 4.—Concluded

| | 117.5W | 107.5 | 97.5 | 87.5 | 77.5 | 67.5 | 57.5 | 47.5 | 37.5 | 27.5 | 17.5 | 7.5W |
|-------|-----------|-------|------|------|---------|--------|-------|------|------|---------|---------|---------|
| 72.5N | • | • | • | • | -19 -11 | -11 -4 | -11 5 | • | • | • | -13 -20 | -14 -13 |
| 67.5N | • | • | • | • | -2 | -10 | • | • | • | -23 -25 | -5 | -11 -5 |
| 62.5N | • | • | • | • | -1 | 6 | 6 | • | • | -10 -23 | -12 -15 | 5 4 |
| 57.5N | • | • | • | • | -8 | 7 | 1 | • | • | -10 -23 | -22 -23 | -1 3 |
| 52.5N | • | • | • | • | -2 | 12 | 6 | 12 | 29 | 44 | 53 | 46 36 |
| 47.5N | • | • | • | • | • | 12 | 28 | 61 | 81 | 71 | 87 | 73 |
| 42.5N | • | • | • | • | 10 | 25 | 41 | 38 | 34 | 35 | 39 | 30 27 |
| 37.5N | • | • | • | • | 21 | 14 | 44 | 68 | 70 | 65 | 72 | 60 57 |
| 32.5N | • | • | • | • | 25 | 37 | 40 | 32 | 21 | 19 | 9 | 8 42 |
| 27.5N | • | • | • | • | 30 | 28 | 24 | 25 | 55 | 51 | 35 | 39 36 |
| 22.5N | -11 -15 | • | • | • | 27 | 34 | 27 | 23 | 43 | 35 | 13 | 3 36 |
| 17.5N | -19 -29 | • | • | • | 14 | 15 | 31 | 35 | 15 | 12 | 9 | 10 17 |
| 12.5N | -23 -21 | • | • | • | 27 | 25 | 29 | 32 | 31 | 14 | 7 | 10 12 |
| 7.5N | -26 -30 | • | • | • | 21 | 20 | 17 | 20 | 14 | -16 | -29 | 23 27 |
| 2.5N | -53 -56 | • | • | • | 24 | 5 | 2 | 14 | -1 | -17 | -67 | -58 -98 |
| 7.5S | -136 -136 | • | • | • | 21 | 22 | 10 | -34 | -18 | -38 | -47 | -44 -60 |
| 12.5S | -19 -40 | • | • | • | 21 | 15 | -5 | -6 | -9 | -8 | -13 | -12 -44 |
| 17.5S | -69 -73 | • | • | • | 21 | 11 | -59 | -80 | -84 | -78 | -94 | -69 -79 |
| 22.5S | -39 -41 | • | • | • | 21 | 15 | -56 | -130 | -58 | -76 | -74 | -32 -47 |
| 27.5S | -93 -92 | • | • | • | 21 | 11 | -37 | -44 | -8 | -50 | -23 | -29 -36 |
| 32.5S | -32 -37 | • | • | • | 21 | 22 | 32 | 4 | • | -17 | -24 | -11 1 |
| 37.5S | -136 -105 | • | • | • | 21 | 20 | -69 | -37 | -38 | -31 | -37 | -30 35 |
| 42.5S | -23 -26 | • | • | • | 21 | 20 | -75 | -64 | -64 | -41 | -41 | -36 45 |
| 47.5S | -117 -117 | • | • | • | 21 | 15 | -15 | -15 | -7 | • | -36 | -40 -45 |
| 52.5S | -69 -73 | • | • | • | 21 | 15 | -92 | -73 | -68 | -101 | -48 | -16 21 |
| 57.5S | -35 -32 | • | • | • | 21 | 15 | -27 | -42 | -43 | -37 | -41 | -33 -39 |
| 62.5S | -14 -14 | • | • | • | 21 | 15 | -42 | -44 | -43 | -44 | -44 | -32 -37 |
| 67.5S | -1 -1 | • | • | • | 21 | 10 | -10 | -11 | -10 | -10 | -10 | -12 -17 |

TABLE 5.—Computed wind stresses, September-October-November. Upper number = τ_u , lower number = τ_v in 10^{-2} dynes cm.⁻²

TABLE 5.—Continued

TABLE 5.—Concluded

| | 117.5W | 107.5 | 97.5 | 87.5 | 77.5 | 67.5 | 57.5 | 47.5 | 37.5 | 27.5 | 17.5 | 7.5W |
|-------|--------|-------|------|------|------|----------|--------|------|------|------|------|------|
| 72.5N | • | • | • | • | • | 12 -11 | 25 -12 | • | • | • | • | -71 |
| 67.5N | • | • | • | • | • | -5 -11 | -6 | • | • | • | -38 | -29 |
| 62.5N | • | • | • | • | • | -65 -109 | • | • | • | • | -41 | -50 |
| 57.5N | • | • | • | • | • | -73 -136 | -83 | • | • | • | -7 | -5 |
| 52.5N | • | • | • | • | • | 81 130 | 58 | • | • | • | -49 | -15 |
| 47.5N | • | • | • | • | • | • | 38 -9 | -83 | -78 | -12 | -13 | -5 |
| 42.5N | • | • | • | • | • | -1 -17 | -40 | -78 | -93 | -62 | -38 | -17 |
| 37.5N | • | • | • | • | • | -8 -14 | -16 | -10 | -12 | -11 | -10 | -3 |
| 32.5N | • | • | • | • | • | 38 42 | 50 | 47 | 54 | 106 | 107 | 114 |
| 27.5N | • | • | • | • | • | -6 -15 | -29 | -25 | 41 | 15 | 35 | 120 |
| 22.5N | 4 | 17 | • | • | • | -10 -15 | -29 | -15 | 44 | 13 | 16 | 127 |
| 17.5N | -37 | -33 | • | • | • | -12 -11 | -3 | -7 | -7 | -14 | -11 | 118 |
| 12.5N | -10 | -56 | 10 | 22 | 9 | -36 -39 | -31 | -29 | -32 | -27 | -32 | 111 |
| 7.5N | -13 | -17 | 3 | -7 | -7 | -39 -35 | -39 | -30 | -32 | -27 | -35 | 97 |
| 2.5N | -38 | -37 | -31 | -27 | -30 | -40 -45 | -43 | -41 | -45 | -41 | -41 | 85 |
| 22.5S | -84 | -99 | -105 | -89 | -86 | -74 -79 | -73 | -63 | -64 | -61 | -61 | 80 |
| 17.5S | -65 | -67 | -74 | -83 | -82 | -87 | -97 | -62 | -52 | -54 | -54 | 74 |
| 12.5S | -22 | -56 | -21 | -50 | -39 | -32 | -36 | -37 | -46 | -59 | -59 | 62 |
| 7.5S | -87 | -76 | -78 | -62 | -52 | -55 | -53 | -33 | -34 | -34 | -34 | 56 |
| 22.5S | -12 | -11 | -15 | -22 | -38 | -29 | -55 | -52 | -21 | -21 | -21 | 53 |
| 27.5S | -19 | -11 | -19 | -19 | -21 | -25 | -34 | -42 | -34 | -34 | -34 | 47 |
| 32.5S | -14 | -10 | -25 | 9 | 30 | 34 | 1 | -87 | -97 | -97 | -97 | 39 |
| 37.5S | 100 | 94 | 36 | 108 | 121 | 130 | 114 | 108 | 122 | 121 | 121 | 125 |
| 42.5S | 105 | 134 | 150 | 161 | 164 | 105 | 156 | 160 | 161 | 112 | 112 | 115 |
| 47.5S | 209 | 205 | 204 | 236 | 301 | 335 | 247 | 251 | 254 | 155 | 154 | 154 |
| 52.5S | 185 | 212 | 240 | 250 | 299 | 340 | 322 | 369 | 351 | 136 | 170 | 175 |
| 57.5S | • | • | • | • | • | • | • | • | • | 158 | 154 | 154 |
| 62.5S | • | • | • | • | • | • | • | • | • | 156 | 144 | 144 |
| 67.5S | • | • | • | • | • | • | • | • | • | 151 | 151 | 151 |

TABLE 6.—Computed wind stresses, annual mean. Upper number = τ_x , lower number = τ_y , in 10^{-2} dynes cm. $^{-2}$

| | 2.5E | 12.5 | 22.5 | 32.5 | 42.5 | 52.5 | 62.5 | 72.5 | 82.5 | 92.5 | 102.5 | 112.5E |
|-------|------|------|------|------|------|------|------|------|------|------|-------|--------|
| 72.5N | 37 | 34 | 10 | -7 | 10 | -24 | 15 | -57 | -60 | -76 | -86 | ... |
| 67.5N | 15 | 29 | 17 | -7 | 11 | -24 | 15 | -57 | -60 | -76 | -86 | ... |
| 67.5N | 40 | 38 | • | • | • | -32 | • | • | • | • | • | • |
| 62.5N | 23 | 30 | • | • | • | -27 | • | • | • | • | • | • |
| 57.5N | 50 | 53 | • | • | • | • | • | • | • | • | • | • |
| 57.5N | 55 | 53 | 24 | • | • | • | • | • | • | • | • | • |
| 52.5N | 69 | 69 | 19 | • | • | • | • | • | • | • | • | • |
| 47.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 42.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 37.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 32.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 27.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 22.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 17.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 12.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 7.5N | • | • | • | • | • | • | • | • | • | • | • | • |
| 2.5N | 8 | 2 | 18 | 18 | 18 | 27 | 25 | 18 | 30 | 24 | 35 | 22 |
| 2.5S | -11 | -11 | • | • | • | 2 | -2 | -15 | -16 | -12 | -4 | 40 |
| 7.5S | -22 | -22 | • | • | • | 18 | 20 | -28 | -27 | 19 | -2 | 28 |
| 7.5S | -25 | -18 | • | • | • | -7 | -36 | -40 | -51 | -48 | -59 | -46 |
| 12.5S | -46 | -34 | • | • | • | -23 | -31 | -74 | -89 | -85 | -104 | -108 |
| 17.5S | -70 | -71 | • | • | • | -22 | -26 | -50 | -57 | -52 | -64 | -67 |
| 22.5S | -48 | -75 | -56 | 96 | • | • | • | -80 | -99 | -101 | -163 | • |
| 27.5S | -64 | -35 | -79 | 123 | • | • | • | • | 55 | 62 | 95 | • |
| 32.5S | 57 | 55 | 75 | • | • | -39 | -36 | -80 | -83 | -64 | -77 | -88 |
| 37.5S | 122 | 90 | 110 | 116 | 91 | 71 | 71 | 76 | 87 | 133 | 107 | 102 |
| 42.5S | 185 | 205 | 232 | 212 | 184 | 140 | 152 | 151 | 179 | 193 | 183 | 192 |
| 47.5S | 250 | 250 | 256 | 228 | 187 | 194 | 203 | 203 | 203 | 216 | 245 | 197 |
| 52.5S | 291 | 258 | 242 | 270 | 270 | 232 | 232 | 232 | 232 | 213 | 204 | 192 |
| 57.5S | • | • | • | • | • | • | • | • | • | 213 | 213 | 213 |
| 62.5S | • | • | • | • | • | • | • | • | • | 213 | 213 | 213 |
| 67.5S | • | • | • | • | • | • | • | • | • | 213 | 213 | 213 |

TABLE 6.—Continued

| | 122.5E | 132.5 | 142.5 | 152.5 | 162.5 | 172.5E | 177.5W | 167.5 | 157.5 | 147.5 | 137.5 | 127.5W |
|-------|------------|------------|-----------|-----------|-----------|-----------|-------------|-------------|-------------|-----------|-----------|-----------|
| 72.5N | • | • | • | • | -11 -12 | -22 -28 | • | -58 | • | -32 -38 | -6 | • |
| 67.5N | • | • | • | • | • | • | • | -38 | -76 | • | • | • |
| 62.5N | • | • | • | • | • | -37 -38 | -23 -68 | -35 -65 | • | • | • | • |
| 57.5N | • | • | • | • | -24 | -14 | -16 -17 | -9 -20 | -11 | 21 | 29 | 8 |
| 52.5N | • | • | • | 33 | 59 -12 | 33 -2 | 23 -19 | 43 -18 | 55 -19 | 68 -24 | 49 -27 | 33 -32 |
| 47.5N | • | • | 48 55 | 88 -6 | 107 -1 | 81 -12 | 72 -19 | 68 -36 | 70 -37 | 78 -73 | 91 -41 | 85 -41 |
| 42.5N | • | • | 58 62 | 83 -10 | 85 -4 | 60 -7 | 69 -17 | 55 -22 | 61 -33 | 64 -32 | 74 -30 | 71 -31 |
| 37.5N | • | • | -36 -11 | 55 -8 | 95 -22 | 61 -6 | 51 -9 | 59 -19 | 60 -30 | 62 -29 | 64 -28 | 62 -20 |
| 32.5N | • | • | -25 -7 | -19 -13 | 23 -15 | 64 -9 | 31 -17 | 36 -22 | 34 -33 | 30 -30 | 28 -17 | 17 -5 |
| 27.5N | -4.2 -6.3 | -9 -7.4 | -24 -4.4 | -20 -2.9 | -19 -1.6 | -10 -1.2 | -19 -1.2 | -8 -4 | -9 -4 | -14 -1.9 | -22 -3.2 | -20 -1.6 |
| 22.5N | -50 -52 | -59 -50 | -36 -53 | -35 -30 | -51 -31 | -49 -23 | -43 -15 | -41 -18 | -37 -26 | -51 -31 | -56 -40 | -53 -38 |
| 17.5N | -4.3 -11.7 | -5.1 -17.5 | -5.1 -5.1 | -5.4 -5.4 | -6.6 -7.1 | -6.6 -7.3 | -6.6 -7.8 | -6.6 -7.3 | -6.6 -7.9 | -6.6 -7.4 | -6.6 -7.5 | -6.6 -7.5 |
| 12.5N | -2.6 -12.5 | -3.3 -2.9 | -2.8 -2.9 | -3.4 -3.0 | -5.1 -5.1 | -6.6 -6.6 | -10.2 -10.1 | -10.2 -11.1 | -11.1 -11.1 | -8.1 -7.9 | -8.1 -7.7 | -8.1 -7.7 |
| 7.5N | -1.2 -7.5 | -1.2 -1.1 | -2.1 -1.1 | -2.7 -1.1 | -5.0 -5.0 | -5.9 -5.9 | -4.9 -5.4 | -4.9 -5.4 | -4.9 -5.4 | -6.4 -7.4 | -6.4 -7.4 | -6.4 -7.4 |
| 2.5N | -1 -2.5 | -1 -1 | -1 -1 | -1 -1 | -2.0 -2.0 | -2.0 -2.0 | -2.0 -2.0 | -2.0 -2.0 | -2.0 -2.0 | -2.0 -2.0 | -2.0 -2.0 | -2.0 -2.0 |
| 2.5S | -1.5 -2.5 | -1.6 -1.8 | -1.3 -1.2 | -1.2 -1.1 | -1.3 -1.2 | -1.3 -1.2 | -1.3 -1.2 | -1.3 -1.2 | -1.3 -1.2 | -1.3 -1.2 | -1.3 -1.2 | -1.3 -1.2 |
| 7.5S | • | • | -32 -32 | -21 -16 | -24 -12 | -24 -8 | -24 -8 | -24 -8 | -24 -8 | -25 -17 | -34 -32 | -34 -32 |
| 12.5S | -1.1 -12.5 | -1.1 -2.7 | -0.4 -0.4 | -0.4 -0.4 | -3.3 -2.1 | -3.7 -2.4 | -3.8 -2.6 | -4.1 -2.6 | -4.1 -2.7 | -3.7 -2.5 | -3.7 -2.5 | -3.7 -2.5 |
| 17.5S | • | • | • | • | • | -4.0 -4.2 | -4.8 -4.8 | -4.8 -4.8 | -4.8 -4.8 | -4.0 -4.0 | -4.0 -4.0 | -4.0 -4.0 |
| 22.5S | • | • | • | • | • | -21 -20 | -19 -19 | -14 -14 | -8 -8 | -29 -30 | -29 -29 | -29 -29 |
| 27.5S | • | • | • | • | • | -35 -26 | -22 -22 | -15 -15 | -13 -13 | -24 -23 | -4 -9 | -9 -12 |
| 32.5S | • | • | • | • | • | 24 -24 | 11 -21 | 11 -13 | 7 -13 | 1 -9 | 17 -12 | 17 -12 |
| 37.5S | 1.0 -1.0 | 8.0 -8.0 | 12.0 -2.4 | 11.8 -1.2 | 11.8 -0.4 | 11.8 -0.4 | 9.8 -1.1 | 9.8 -1.1 | 9.8 -1.1 | 10 -1.1 | 10 -1.1 | 10 -1.1 |
| 42.5S | -1.7 -4.2 | 13.5 -10.1 | 14.3 -2.4 | 14.2 -1.2 | 13.7 -0.4 | 11.8 -0.4 | 11.8 -0.4 | 11.8 -0.4 | 11.8 -0.4 | 11.8 -0.4 | 11.8 -0.4 | 11.8 -0.4 |
| 47.5S | 2.3 -2.5 | 20.2 -8.0 | 20.2 -1.0 | 16.9 -0.0 | 16.9 -0.0 | 16.9 -0.0 | 14.4 -0.4 | 14.4 -0.4 | 14.4 -0.4 | 12.2 -0.4 | 12.2 -0.4 | 12.2 -0.4 |
| 52.5S | • | • | • | • | • | 15.4 -2.3 | 16.8 -1.2 | 19.5 -0.4 | 17.3 -0.4 | 19.0 -0.4 | 15.2 -0.4 | 19.4 -0.4 |
| 57.5S | • | • | • | • | • | 15.4 -2.3 | 16.8 -1.2 | 19.5 -0.4 | 17.3 -0.4 | 19.0 -0.4 | 15.2 -0.4 | 19.4 -0.4 |
| 62.5S | • | • | • | • | • | 15.4 -2.3 | 16.8 -1.2 | 19.5 -0.4 | 17.3 -0.4 | 19.0 -0.4 | 15.2 -0.4 | 19.4 -0.4 |
| 67.5S | • | • | • | • | • | 15.4 -2.3 | 16.8 -1.2 | 19.5 -0.4 | 17.3 -0.4 | 19.0 -0.4 | 15.2 -0.4 | 19.4 -0.4 |

TABLE 6.—Concluded